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# A MILP Framework to Solve the Sustainable System Optimum with Link MFD Functions

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#### SHORT SUMMARY

Given the increasing consciousness toward the environmental footprint of mobility, accommodating environmental objectives in existing transport planning strategies is imperative for research and practice. In this paper, we use the link macroscopic fundamental diagram (MFD) model to develop optimal routing strategies that minimize total system emissions (TSE) in multiple origin-destination (OD) networks. Piecewise linear (PWL) functions are used to approximate MFD for individual links, and to define link-level emissions. Dynamic network constraints, non-vehicle holding constraints, and convex formulations of the PWL functions are considered. Thus, the system-optimum dynamic traffic assignment (SO-DTA) problem with environmental objectives is formulated as a mixed integer linear program (MILP). Finally, on a synthetic network, numerical examples demonstrate the performance of the proposed framework.

Keywords: traffic assignment, system optimum, macroscopic fundamental diagram, emissions

# 1. INTRODUCTION

Congestion in transportation networks and its eminent environmental effects are becoming imperative issues in recent times. In this regard, optimal routing strategies are emerging as viable solutions to improve transportation network management and tackle these issues. Environmental objectives should be considered at the network level. Sustainable System Optimum (SSO) is thus a special case of the SO-DTA (Sheffi, 1984) where the minimization process targets the emissions instead of the total travel time.

To solve the SSO while considering traffic dynamics, we employ discrete-time analytical SO-DTA models that are mostly formulated as linear programming (LP) and mixed integer linear programming (MILP) problems (e.g., Ziliaskopoulos, 2000; Aziz and Ukkusuri, 2012; Long et al., 2018). Based on objectives, the existing SO-DTA models can be categorized into two main groups: minimizing total system travel time (TSTT)(e.g., Ghali and Smith, 1995; Ziliaskopoulos, 2000; Long and Szeto, 2019), and minimizing total system emissions (TSE)(e.g., Aziz and Ukkusuri, 2012; Long et al., 2018). Throughout the literature, it is evident that most existing SO-DTA models are concerned with the TSTT. Built upon linear and convex functions, such objectives have advantages such as being computationally efficient for reasonably sized networks. On the other hand, few studies have attempted to address the TSE in the SO-DTA model. Their

main limitations reside in the computational performance due to the nonlinear and nonconvex objective functions, as well as in the contextual applicability due to solely examining simplified single OD networks.

This study extends the MILP framework for solving TSTT by Shakoori et al. (2022) to address the TSE on multiple OD networks. We adopt the PWL link-MFD functions to describe link-level traffic dynamics. So, each link can be represented by a single cell characterized by its density. The link-MFD characterizes the effect of traffic control and the different states that a link between two intersections can encounter. From the PWL link MFDs, we further derive the PWL link emissions to tackle the non-linear TSE objective function. Additionally, we investigate the challenges for TSE optimization and study multiple alternatives to improve the computational efficiency of the proposed framework such as reducing the dimensionality of the problem and path selection strategies. The remainder of this paper is organized as follows. Section 2 presents the methodological framework. Section 3 provides a case study, numerical results, and discussions.

# 2. METHODOLOGY

In this section, we present a MILP framework for modeling a link-based TSE-SO-DTA. Table 1 resumes the adopted nomenclature.

**Table 1: Notations** 

Notation	Description
T	Set of discrete time intervals
$\Delta t$	Time interval duration
$C_R$	Set of origin links
$C_S$	Set of destination links
С	Set of links except for the destination links
$Q_i^t$	The maximum flow that can get into or out of link $i$ at time interval $t$
$egin{aligned} Q_i^t \ l_i \end{aligned}$	Length of link i
$d^{O,D,t}$	Demand from origin O to destination D at interval t
$x_i^{O,D,t}$	Number of vehicles in link $i$ during time $t$ oriented from origin O headed to destination D
$y_{i,j}^{O,D,t}$	Number of vehicles moving from link $i$ to link $j$ during time $t$ from origin O to destination D
$k_i^{O,D,t}$	OD Segregated density of link $i$ at time $t$
$k_i^t$	Aggregated density of link $i$ at time $t$
$\Gamma(i)$	Set of successor links of link <i>i</i>
$\Gamma(i)^{-1}$	Set of predecessor links of link <i>i</i>
$\Gamma(i)^{O,D}$	Set of successor links of link $i$ on the paths from origin O to destination D
$\Gamma(i)^{-1,O,D}$	Set of predecessor links of link $i$ on the paths from origin O to destination D
$D(k_i^t)$	Aggregated demand in link $i$ during time t as a function of density
$D(k_i^{O,D,t})$	Segregated demand in link $i$ from origin O to destination D during time t as a function of density
$S(k_i^t)$	Aggregated supply at cell $i$ during time $t$ as a function of density

# 2.1. Piecewise Linear Link Macroscopic Fundamental Diagram

As depicted in Figure 1, we approximate the link MFDs by PWL functions. Accordingly, the PWL demand (branches *I,II, and III*, and *VIII*) and supply functions (branches *VII,IV,V,VI*) can be defined by their breakpoints by employing a convex combination formulation and a set of variables, known as the special ordered sets of type 2 (SOS2) in

which at most two variables can be positive, and if two are positive they must be consecutive (Keha et al., 2004; Beale and Tomlin, 1969)

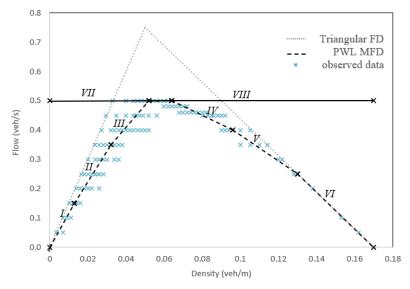


Figure 1. Link-level MFD, triangular FD approximation, and its PWL MFD counterpart

Given the B breakpoints on the PWL demand function as  $(k_{i,b}^{O,D,t}, F_{i,b}^{O,D,t})$  for  $b \in \{1, ..., B\}$ , for each link i and each OD pair at time t we can write (Shakoori et al., 2022):

$$k_i^{O,D,t} = \sum_{b=1}^{B} k_{i,b}^{O,D,t} \times \lambda_{i,b}^{O,D,t}$$
 (1a)

$$D(k_i^{O,D,t}) = \sum_{b=1}^{B} F_{i,b}^{O,D,t} \times \lambda_{i,b}^{O,D,t}$$
 (1b)

where 
$$\sum_{b=1}^{B} \lambda_{t,b}^{O,D,t} = 1$$
 (2a)

$$\lambda_{i,b}^{0,D,t} \ge 0 \ \forall b \in \{1, \dots, B\}$$
 (2b)

$$\lambda_{i,b}^{0,D,t} \ b \in \{1, ..., B\} \text{ is SOS2}$$
 (3)

 $D(k_i^{O,D,t})$  is the OD segregated demand at link i during time t. For the aggregated demand at link i during time t one can write:

$$D(k_i^t) = D(\sum_{O,D} k_i^{O,D,t}) \tag{4}$$

# 2.2. Link MFD-based Dynamic Network Constraints

Analytical description of traffic model in link MFD-based TSE-SO-DTA problem requires introducing a set of constraints to the MILP framework. This includes the initial state of the network, the mass flow conservation, flow propagation relations, and non-vehicle holding (NVH) conditions. We adopt the same set of discrete-time MILP constraints introduced by Shakoori et al. (2022):

$$x_{i}^{O,D,0} = 0, \ y_{i,j}^{O,D,0} = 0 \qquad \forall i \in C, \forall j \in C, \forall O \in C_{R}, D \in C_{S} \qquad (5)$$
 
$$x_{i}^{O,D,t} \geq 0, \ y_{i,j}^{O,D,t} \geq 0 \qquad \forall i \in C \cup C_{S}, \forall O \in C_{R}, D \in C_{S}, t \in T \qquad (6)$$
 
$$x_{i}^{O,D,t} - x_{i}^{O,D,t-1} + \sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t-1} = d^{O,D,t-1} \qquad \forall i \in C_{R}, D \in C_{S}, \forall t \in T \qquad (7)$$
 
$$x_{i}^{O,D,t} - x_{i}^{O,D,t-1} - \sum_{k \in I^{-1,O,D}(i)} y_{k,i}^{O,D,t-1} = 0 \qquad \forall i \in C \setminus C_{R}, D \in C_{S}, \forall t \in T \qquad (8)$$
 
$$\sum_{O,D} \sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{t}) \times \Delta t \qquad \qquad O \in C_{R}, D \in C_{S}, t \in T \qquad (8)$$
 
$$\sum_{O,D} \sum_{k \in I^{-1,O,D}(i)} y_{k,j}^{O,D,t} \leq S(k_{j}^{t}) \times \Delta t \qquad \qquad O \in C_{R}, D \in C_{S}, \forall j \in I^{(i)} \qquad (10)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in T, O \in C_{R}, D \in C_{S} \qquad (11)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in T, O \in C_{R}, D \in C_{S} \qquad (11)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in T, O \in C_{R}, D \in C_{S} \qquad (11)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in T, O \in C_{R}, D \in C_{S} \qquad (11)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in C, \forall t \in T \qquad (12)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in C, \forall t \in T \qquad (12)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in C, \forall t \in T \qquad (13)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in C, \forall t \in T \qquad (14)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in C, \forall t \in T \qquad (14)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in C, \forall t \in T \qquad (14)$$
 
$$\sum_{j \in I^{O,D}(i)} y_{i,j}^{O,D,t} \leq D(k_{i}^{O,D,t}) \qquad \forall t \in C, \forall t \in T \qquad (14)$$

where M is a very large positive value,  $G_i = \{1, 2, ..., |\Gamma(i)|\}$  is an index set for link i's successor links,  $j_g$  is the g-th link in  $\Gamma(i)$ ,  $m_i = \operatorname{argmin}_m \{2^{m+1} \geq 2 + 2 \times |\Gamma(i)|\}$ , and  $\sigma_a^g$  is 0 or 1, such that  $\sum_{a=1}^{m_i} 2^{a-1} \times \sigma_a^g = g$ .

The initial state of the network is captured in equation (5). Equation (6) ensures the non-negativity of the variables. The link mass conservation is guaranteed by equations (7)-(8). Equations (9)-(11) represent the flow propagation constraints. Equations (12)-(15) ensure the NVH conditions.

# 2.3. Link MFD-based SO-DTA models in terms of Total System Emission (TSE)

In a TSE-SO-DTA we are seeking to minimize the network-level pollutant emission which can be obtained by the sum of links' emissions during the simulation period. The objective function then reads:

$$\min_{x_i^t} TSE = \sum_{i \in C} \sum_{t \in T} E_i^t \tag{16}$$

 $E_i^t$  represents link emission and can be calculated as the product of (i) total traveled distance (TTD) of all vehicles on the link and (ii) emission factor (EF) modeled as a function of mean speed according to the COPERT model (EMISIA, 2022). Therefore:

$$E_i^t = TTD \times EF = \Delta T \times x_i^t \times V(x_i^t) \times EF(V(x_i^t))$$
(17)

A polynomial regression model is used to compute the  $CO_2$  emission factor as a function of speed for an aggregated vehicle representing the entire French vehicle fleet (fleet composition data in Citepa (2017)):

$$EF(V(x_i^t)) = p_4 V(x_i)^4 + p_3 V(x_i)^3 + p_2 V(x_i)^2 + p_1 V(x_i) + p_0$$
(18)

The coefficients of the regression model (i.e.,  $p_4$ ,  $p_3$ ,  $p_2$ ,  $p_1$ , and  $p_0$ ) were estimated from speed-emission data.

For any given density, considering traffic demand constant during each time step, the mean speed and the emission factor can be calculated from (18). This implies that for every breakpoint on the PWL link MFD, knowing the mean speed ( $speed = \frac{flow}{density}$ ), the corresponding emission factor can be calculated from (18). The link emission then is obtained from (17) allowing us to derive a PWL link emission function from the PWL link MFD.

Representing the link emissions as a PWL function of the link density is again achieved by using SOS2 constraints and a convex combination of the breakpoints  $(k_{i,b_e}^t, E_{i,b_e}^t)$  for  $b_e \in \{1, ..., B_e\}$  where  $B_e$  is the number of breakpoints on emission function and thus a model parameter:

$$k_i^t = \sum_{b_e=1}^{B_e} k_{i,b_e}^t \times \gamma_{i,b_e}^t$$
 (19a)

$$E_{i}^{t} = \sum_{b_{e}=1}^{B_{e}} E_{i,b_{e}}^{t} \times \gamma_{i,b_{e}}^{t}$$
(19b)

where 
$$\sum_{b_e=1}^{B_e} \gamma_{i,b_e}^t = 1$$
 (20a)

$$\gamma_{i,b_e}^t \ge 0 \ \forall b_e \in \{1, \dots, B_e\}$$
 (20b)

$$\gamma_{i,b_e}^t \ b_e \in \{1, \dots, B_e\} \text{ is SOS2}$$
 (21)

The MILP formulation of TSE-SO-DTA then reads:

$$\min_{x_i^t} TSE = \sum_{i \in C} \sum_{t \in T} E_i^t \tag{22}$$

Subject to: constraints 
$$(1) - (15)$$
 and constraints  $(19) - (21)$ 

In comparison to the TSTT with a linear objective function, the PWL objective of the TSE problem induces additional complexity due to the increased number of variables and constraints. Also, such objective functions make the NVH constraints, that are responsible for preventing trivial and suboptimal solutions, even more necessary as discussed later on. Therefore, specific arrangements are needed to preserve a computational burden compatible with practical applications.

# 3. RESULTS AND DISCUSSION

# 3.1. Simulation Setting

The suggested framework is implemented on a small network similar to the Nguyen and Dupuis (1984) network, as illustrated in Figure 2, with 6 OD pairs. 2 scenarios are considered. In scenario 1, the demand for each OD pair (d=0.2 veh/s) is lower than the maximum capacity allowing vehicles to travel at free-flow speed. In scenario 2, the demand is increased (d=0.4 veh/s) to make the network congested yet without gridlocks. The simulation is carried out for 2 minutes.

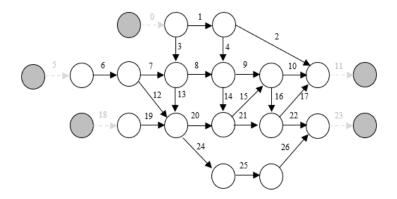


Figure 2. Simulated network

For the demand function, the first and last breakpoints of link i are (0,0) and  $(k_{jam}^i, Q_i)$  respectively. For the supply function, they are  $(0,Q_i)$  and  $(k_{jam}^i,0)$ . Characteristics and other breakpoints for each link are summarized in Table 2. Jam density is set to 0.17 vehicles/m for all links.

Table 2: Characteristics of the links in the simulated network

Link 1 2 3	(m) 250 400 250	(veh/s) 0.5 0.3	(m/s) 12.5		Demand function	1		C1 C	
	400		12.5	(0.02.0.25)				Supply function	1
		0.3		(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
2	250	0.0	14	(0.01, 0.14)	(0.02, 0.25)	(0.0265, 0.3)	(0.11, 0.3)	(0.13, 0.23)	(0.15, 0.13)
3		0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
4	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
6	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
7	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
8	250	0.3	12.5	(0.01, 0.125)	(0.02, 0.2)	(0.04, 0.3)	(0.06, 0.3)	(0.1, 0.23)	(0.14, 0.12)
9	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
10	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
12	300	0.5	15	(0.01, 0.15)	(0.03, 0.38)	(0.05, 0.5)	(0.07, 0.5)	(0.1,0.4)	(0.14, 0.2)
13	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
14	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
15	300	0.5	15	(0.01, 0.15)	(0.03, 0.38)	(0.05, 0.5)	(0.07, 0.5)	(0.1,0.4)	(0.14, 0.2)
16	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
17	300	0.5	15	(0.01, 0.15)	(0.03, 0.38)	(0.05, 0.5)	(0.07, 0.5)	(0.1,0.4)	(0.14, 0.2)
19	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
20	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
21	250	0.3	12.5	(0.01, 0.125)	(0.02, 0.2)	(0.04, 0.3)	(0.06, 0.3)	(0.1, 0.23)	(0.14, 0.12)
22	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
24	300	0.5	15	(0.01, 0.15)	(0.03, 0.38)	(0.05, 0.5)	(0.07, 0.5)	(0.1, 0.4)	(0.14, 0.2)
25	250	0.5	12.5	(0.02, 0.25)	(0.04, 0.4)	(0.06, 0.5)	(0.08, 0.5)	(0.12, 0.35)	(0.14, 0.24)
26	300	0.5	15	(0.01, 0.15)	(0.03, 0.38)	(0.05, 0.5)	(0.07, 0.5)	(0.1, 0.4)	(0.14, 0.2)

#### 3.2. Results

First, we investigate the trade-off between TSTT and TSE when each of them is considered as the objective function. The results are summarized in Table 3.

Table 3: TSTT and TSE Trade-off

Scenario 1: 2 minutes of simulation, demand=0.2 veh/s					
Objective	TSTT(s)	TSE(g)			
Minimizing TSTT	7018	7730			
Minimizing TSE	7200	7218			

Scenario 2: 2 minutes of simulation, demand=0.4 veh/s

Objective	TSTT(s)	TSE(g)
Minimizing TSTT	14143	14629
Minimizing TSE	14399	14074

As expected, in case of a higher level of demand the total system travel time and emission values are increased.

The TSE optimization yields the minimum  $CO_2$  emission, but with a higher travel time in comparison to the optimal travel time achieved in the TSTT optimization. The TSE model does not allow the speed values to reach the highest possible most of the time to save  $CO_2$  emissions. As a result, the system-wide travel time is higher for the whole network. Lower TSTT comes at the cost of a higher level of TSE and vice versa.

Second, we compare the results for both TSTT and TSE problems with and without NVH constraints to further scrutinize how they affect the optimization and the solutions. Results are presented in Table 4.

Table 4: Comparison of Results with and without NVH

2 minutes of simulation, demand=0.4 veh/s						
	TS	TT	TSE			
_	Objective	Calculation	Objective	Calculation		
	value(s)	time(s)	value(g)	time(s)		
With NVH	14143	6	14074	905		
Without NVH	14169	3	11585	17		

As already mentioned, the NVH constraints play a more important role when solving for TSE. They prevent trivial and under-estimated solutions with vehicles staying put to reduce emissions. Their importance, however, becomes less significant in the TSTT problem. This is mainly because vehicles moving along their paths and getting to their destinations as soon as possible contribute to reducing TSTT. This implies the incentive of vehicles to move forward rather than holding back even in the absence of NVH constraints when solving for TSTT.

Despite the importance of the NVH constraints, they increase the calculation time noticeably, especially for the TSE problem. To alleviate the calculation burden, we study several alternatives. We analyze the sensitivity of the results and solution algorithm to the number of breakpoints on the PWL emission function. A path selection strategy is also implemented in which only two alternative paths for each OD pair are accessible to the users of the network. In Table 5 some initial results are presented.

**Table 5: Sensitivity Analysis to Number of Breakpoints and Path Selection** 

2 minutes of simulation, demand=0.4 veh/s, with NVH constraints						
BP	All p	ossible paths	Path selection			
	TSE(g)	Calculation time(s)	TSE(g)	Calculation time(s)		
8	14074	905	14195	10		
6	13755	108	14119	7		
4	13209	22	13761	4		

Increasing the number of breakpoints (BP) on the PWL emission function increases the accuracy of the solution and prevents sub-optimality. However, this comes at the cost of higher calculation time stemming from the increased complexity of the solution algorithm to take into account more breakpoints and corresponding variables and constraints.

The computational burden can be further decreased by employing path selection strategies. Results suggest a significant decrease in calculation time when the set of feasible paths for each OD is restricted to the first and second shortest path.

We are currently investigating different alternatives to further tackle the computational challenges. Those results will be presented at the MFTS 2022 conference.

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